

279 HILL STREET, PORT STANLEY

MUNICIPALITY OF CENTRAL ELGIN

PRELIMINARY SERVICING AND STORMWATER MANAGEMENT REPORT



19084 13 April 2021 Rev. 29 March 2022

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19084



CYRIL J. DEMEYERE LIMITED

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PRELIMINARY SERVICING AND STORMWATER MANAGEMENT REPORT

1.0 Introduction

The property at 279 Hill Street is located on the northeast side of Port Stanley, west of the intersection of Hill Street and East Road (County Road 23). The site is 0.81 ha of land, currently occupied by a single residence with a gravel driveway. The property owner of 279 Hill Street intends to develop the site as an infill residential development. The development proposal includes constructing six 4-unit townhouse buildings and one 3-unit townhouse, for a total of 27 units, fronting an internal private access road and associated surface level parking.

The site is relatively flat, with the property generally draining westerly over the existing bluff and southerly into the ravine adjacent to Hill Street, at the top end of the Siebenmorgen Municipal Drain, all of which eventually outlets to Kettle Creek. The site falls under the jurisdiction of the Kettle Creek Conservation Authority.

This report has been prepared for the Developer of 279 Hill Street, Morgan Pavia, for the purposes of accompanying the second submission of Zoning By-Law Amendment (ZBA) and concurrent Draft Plan of Condominium applications for the subject lands. Please refer to the Site Plan (Drawing 1) and the Preliminary Servicing Plan (Drawing 3), enclosed in Appendix A.

2.0 Geotechnical Investigation

The native soil at the site is predominantly comprised of silty clay till as witnessed by a Geotechnical Investigation and Slope Assessment Report (MTE, 15 December 2020). The soil has a relatively low permeability, therefore is generally unsuitable for groundwater recharge.

The valley which contains the Siebenmorgen Drain varies in size and slope in the vicinity of the subject lands. At the southern limits of 279 Hill Street, the valley is 5m deep with an approximate side slope inclination of 2:1 (H:V).

At the northwest corner of the property the top of bank of a 31m high slope is approximately 20m from the nearest proposed townhouse. The inclination of this slope is approximately 3:1 (H:V). The Slope Assessment Report concluded that the valleylands have a slope instability rating of "low potential" requiring a "site inspection only, confirmation, and report letter".



Refer to Geotechnical Investigation and Slope Assessment Report (MTE, 15 December 2020) for further details on the subsurface conditions and slope assessment.

3.0 Sanitary Sewage

"Sunset Road Sanitary Sewer Extension: Tributary Service Area Analysis" (CJDL, 8 September 2015) was completed to study the design sanitary servicing tributary areas to the proposed Sunset road (County Road No. 4) sanitary sewer extension, including Sunset Bluffs Subdivision and surrounding area (incl. 279 Hill Street lands). In accordance with recommendations of the study, in spring 2016 the trunk sanitary sewer extension on Sunset Road (County Road No. 4) was constructed to provide a sanitary sewer outlet for Sunset Bluffs Subdivision and surrounding area.

The 200mmø sewer was since extended southerly on Larry Street, on Hill Street (from East Road to High Street), and southerly on High Street in summer 2020 concurrent with development of the Landings Port Stanley Subdivision. To provide sanitary service to 279 Hill Street, a 90±m long sanitary sewer extension on Hill Street, west from High Street is required, and is anticipated to include associated road reconstruction along Hill Street.

The 279 Hill Street property is within the design tributary area for the proposed 200mmø Hill Street sewer. Design flows have been evaluated to consider the proposed 27 residential townhouse units at 279 Hill Street. At 3.5 people/unit (Pop = 95), the Hill Street sanitary sewer and its outlet at Larry Street have sufficient capacity to service the proposed development at 279 Hill Street. The existing sewer stub has been installed to provide gravity basement drainage to all proposed townhome units.

4.0 Storm Drainage

4.1 Existing Site Conditions

The site is relatively flat, with the property generally draining westerly over the existing bluff and southerly into the ravine adjacent to Hill Street, at the top end of the Siebenmorgen Municipal Drain, all of which eventually outlets to Kettle Creek. The site currently includes a single family residence, gravel driveway, and associated accessory buildings, equating to approximately 8% impervious level and a pre-development run-off coefficient of C = 0.38. In post-development conditions, the run-off is increased to C = 0.70, reflective of the increased level of site imperviousness of proposed buildings and asphalt roadway. Refer to Appendix B for calculations.

Referring to the Seibenmorgen Drain (Spriet Associates, 1981) drawing included in Appendix A, approx. 0.52 ha of the 0.81 ha site is currently tributary to the Siebenmorgen Drain, via the existing ravine north of Hill Street, developing at the westerly limit to the existing driveway at 279 Hill Street.

Storm sewers are not present on Hill Street west of 279 Hill Street, and rather surface run-off discharges directly to the existing ravine on the north side of Hill Street, prior to discharge to the Siebenmorgen Municipal Drain. Although intermittent catchbasins with informal outlet treatments have been installed by the Municipality over the years to varying degrees of effectiveness, concentrated flows over the ravine bank appear to remain a cause of erosion. Concurrent with eventual storm sewer construction at 279 Hill Street, it is proposed that surface flows at the most problematic areas of the Hill Street ravine will be re-routed to a common outlet, at the confluence of the existing Beamish Street drain and the proposed 279 Hill Street storm sewer. A proper outlet headwall structure and cable concrete matting for erosion control is proposed to help alleviate existing erosion concerns along the ravine side slopes.



4.2 Stormwater Management Concept

The storm drainage outlet for the site will be the Hill Street ravine, and eventually the Siebenmorgen Municipal Drain. It is proposed that stormwater from the 279 Hill Street development will outlet to a new storm manhole, prior to discharge to Kettle Creek at the entrance to the site, which will also act as the outlet for the sewer improvements proposed by Central Elgin and the Hill Street Municipal Drain, as described in the section above.

It is proposed that post-development discharge from the site (0.81± ha @ C = 0.70) will be restricted to pre-development run-off from the site, for up to the 100-year storm event, in accordance with Municipality of Central Elgin Design Guidelines and MECP accepted stormwater management (SWM) practices.

Site Plan design for the development includes a proposed 'StormTech SC-740 Chamber' to provide both quantity and quality control of the effluent storm water. This underground storage facility will be located in the proposed access road at the entrance of the site and has been selected for use in this application to not conflict with other proposed underground infrastructure, while still ensuring that the necessary SWM requirements are met. Refer to Appendix 'B' for further product information.

Quantity control for the 5 to 100-year design storm will be provided via a 150mmø orifice plate at the outlet of the underground storage chamber. Refer to Appendix 'A' for Post-Development Flow Calculations, and as summarized by the following Table 1.

Design Storm	5-Year	100-Year
Pre-Development Outflow (I/s) Tributary Area = 0.81 ha	46.5	105.8
Post-Development Outflow (I/s) Tributary Area = 0.81 ha	41.6	65.9
Storage Required (m ³)	78	182
Storage Provided (m ³)	190	190
Max. Water Elev. in SWM Chamber (m)	210.26	210.85

Table 1 - Stage-Storage-Discharge Relationship

It is therefore demonstrated that sufficient storage is provided within proposed underground SWM chamber to control post-development flows from the Site to pre-development levels.

5.0 <u>Watermain</u>

The existing Port Stanley elevated storage tank is located northeast of the subject 279 Hill Street property, at the intersection of Dexter Line and East Road. An existing 300mmø trunk watermain runs south from the Port Stanley water tower along the west side of East Road. An existing 250mmø watermain runs from East Road westerly along Hill Street and connects to an existing 200mmø watermain on Colborne Street/Sunset Drive.



The 2000 Dillon Water and Sanitary Servicing and Traffic/Roads Report concluded that there is sufficient available capacity in the existing trunk watermains on Hill Street, East Road and Dexter Line to service the near-term development area which included the Little Creek Subdivision and surrounding Beamish/Larry/Hill Street development areas.

The existing 250mmø watermain along Hill Street can provide water service to the site. One (1) 200mmø point of connection is proposed to provide water service to the two (2) fire hydrants and the seven (7) buildings proposed within the development. Individual 25mmø water services will be provided to each unit from the proposed 200mmø internal watermain.

6.0 Electrical and Utilities

279 Hill Street is currently within the electrical service area of Hydro One Networks Inc. (HONI). It is anticipated that HONI will be the electrical service provider for the proposed development.

Bell, Rogers and Engbridge also provide utility service to this area Port Stanley, and it is further anticipated that they will have adequate capacity on Hill Street to service the proposed development.

Street lights will be designed to Municipality of Central Elgin design criteria, ensuring that light trespass to neighbouring properties will be minimized and that a detailed lighting distribution plan will be provided as part of the Site Plan Application package. The classification of roadways and their recommended luminance light levels will be as per IESNA RP-8-14 and TAC 2006 Guide for the Design of Roadway Lighting.

7.0 Traffic

Vehicular connection for the 27 units at the site will have one (1) point of access provided from Hill Street at the southern limit of the site. The Traffic Impact Assessment by F. R. Berry & Associates (January 2022) concluded that the proposed development at 279 Hill Street will have no significant impact on the operation of the intersection of Hill Street and East Road (County Road 23).

The development will provide a parking supply of 54 off-street parking spaces, including driveways and garages, which meets the zoning requirement of 1.5 off-street parking spaces per unit.

8.0 Natural Heritage

An Issue Scoping Report was completed by Vroom + Leonard (formerly Leonard & Associates) in June 2020 (Rev. April 2022). The report concluded that the proposed development of the site does not pose any potential issues from a natural heritage perspective as long as the recommended mitigative measures noted in the report are followed. A full Environmental Impact Study (EIS) is not required for the site.

9.0 Other Related Studies

The following related studies have been prepared in support of the proposed Zoning By-Law Amendment application:

- Planning Justification Report, Zelinka Priamo (Rev. May 2022)
- Archaeological Assessment, Lincoln Environmental Consulting Group (November 2020)



Please refer to the aforementioned reports for further information on their respective topics.

** ** **

All of which is respectfully submitted by,

Ven Mple (1

Cameron Cluett, P. Eng.

Deren Lyle, P. Eng.

CJC/kc



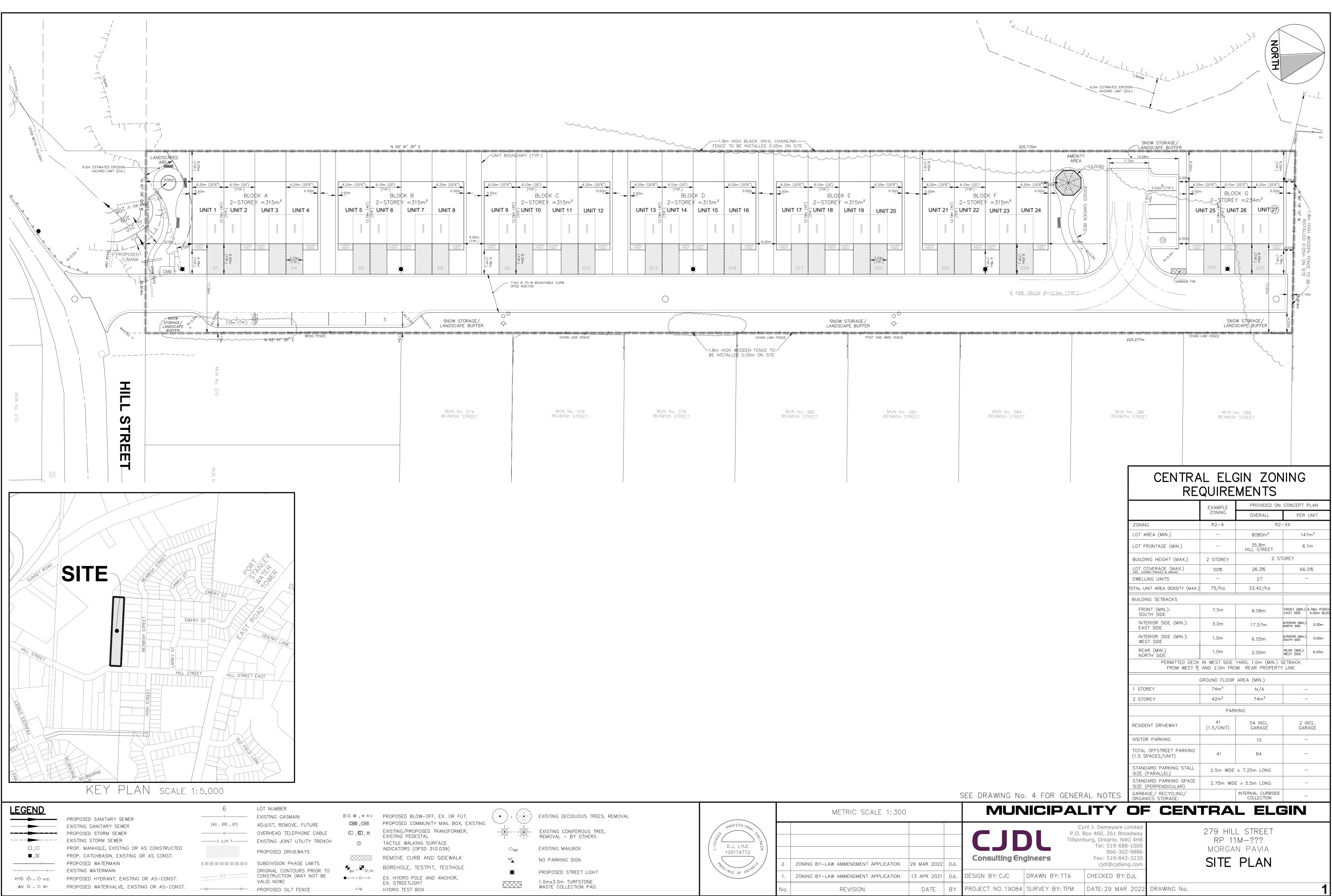
APPENDIX 'A' - DRAWINGS

DRAWING 1 - SITE PLAN (29 MARCH 2022)

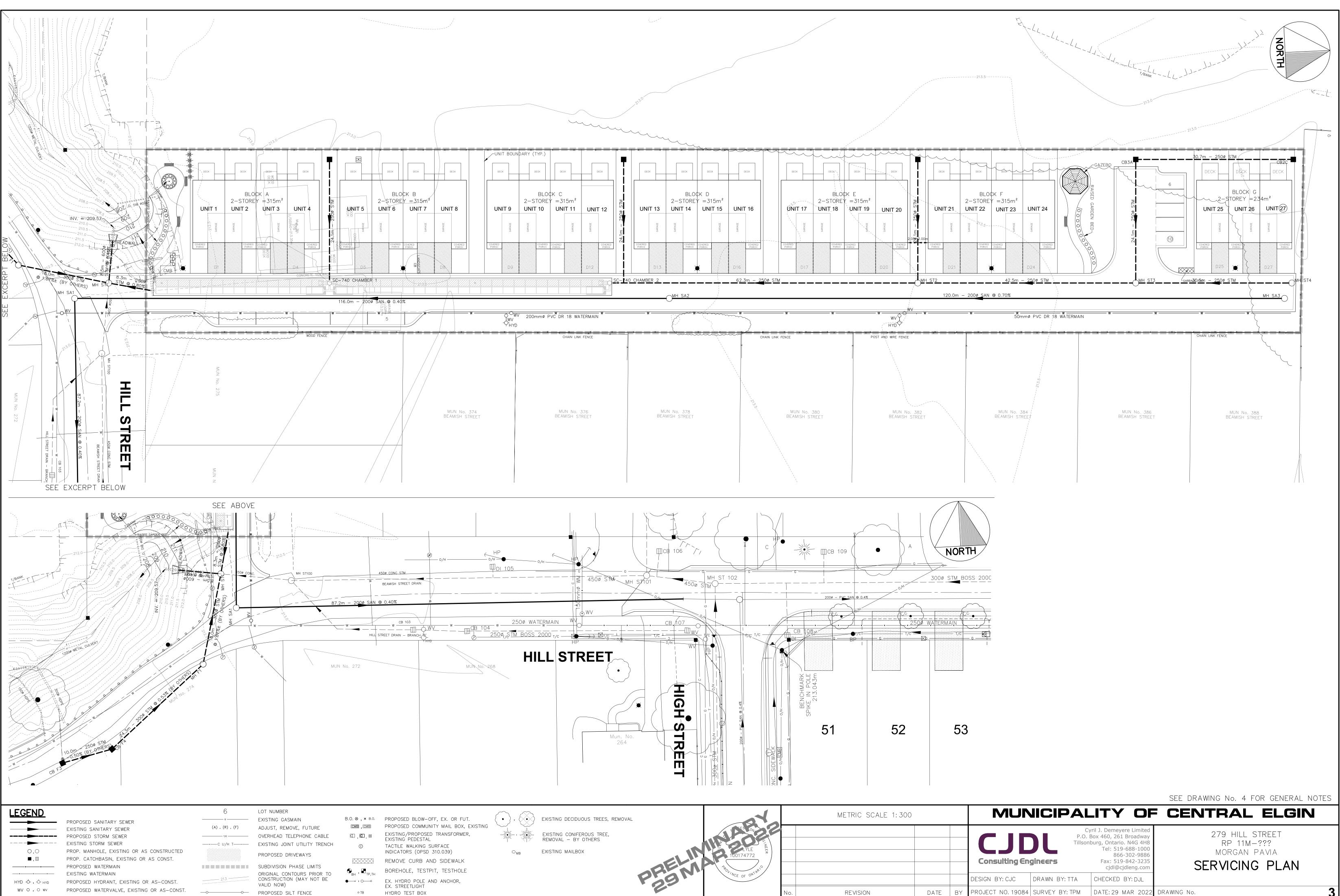
DRAWING 3 - SERVICING PLAN (29 MARCH 2022) - PRELIMINARY

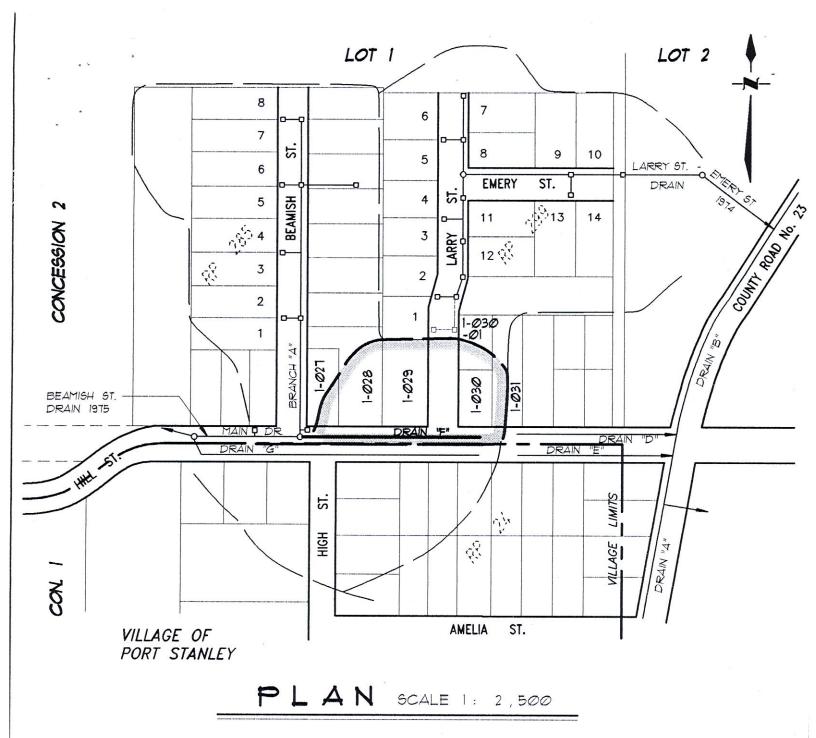
Municipal Drain & Storm Sewer Reference Drawings:

- Hill Street Drain (Spriet Associates, 1997)
- Siebenmorgen Drain (Spriet Associates, 1981)



FUT.	(•), 🐼	EXISTING DECIDUOUS TREES, REMOVAL			METRIC SCALE 1:300	
BOX, EXISTING RMER,		EXISTING CONIFEROUS TREE, REMOVAL – BY OTHERS	PROFESSIONAL CL			
	O _{MB}	EXISTING MAILBOX	D.J. LYLE 100174772			
alk Iole	NP	NO PARKING SIGN	PROLINCE OF ONTRE	2.	ZONING BY-LAW AMMENDMENT APPLICATION	29 MAR 202
R,	X	PROPOSED STREET LIGHT 1.0mx3.0m TURFSTONE	NCE OF ON	1.	ZONING BY-LAW AMMENDMENT APPLICATION	13 APR 20
		WASTE COLLECTION PAD		No.	REVISION	DATE



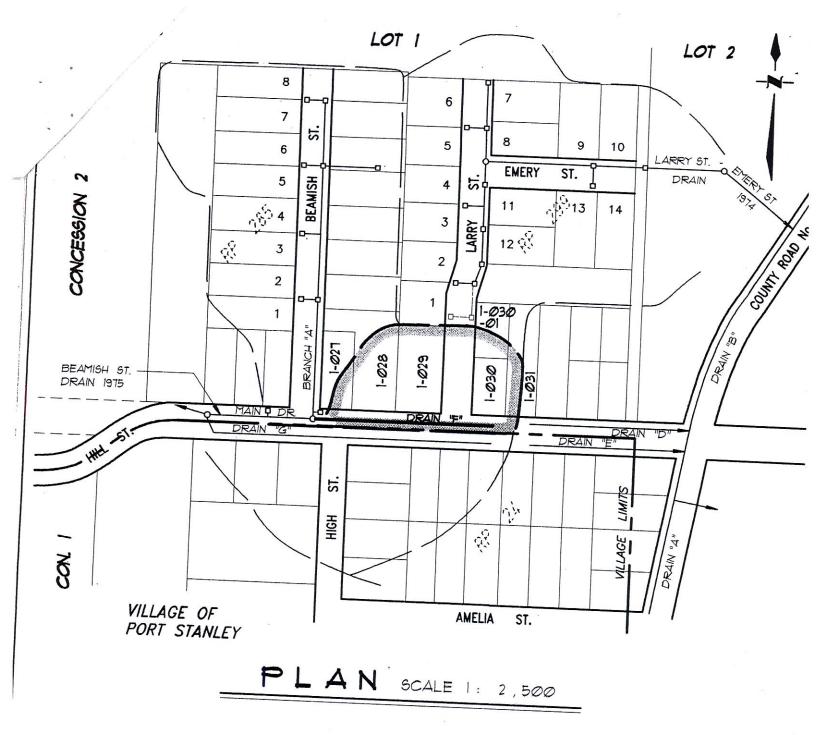


PLAN

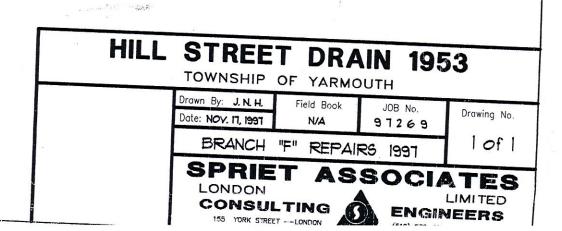
LEGEND

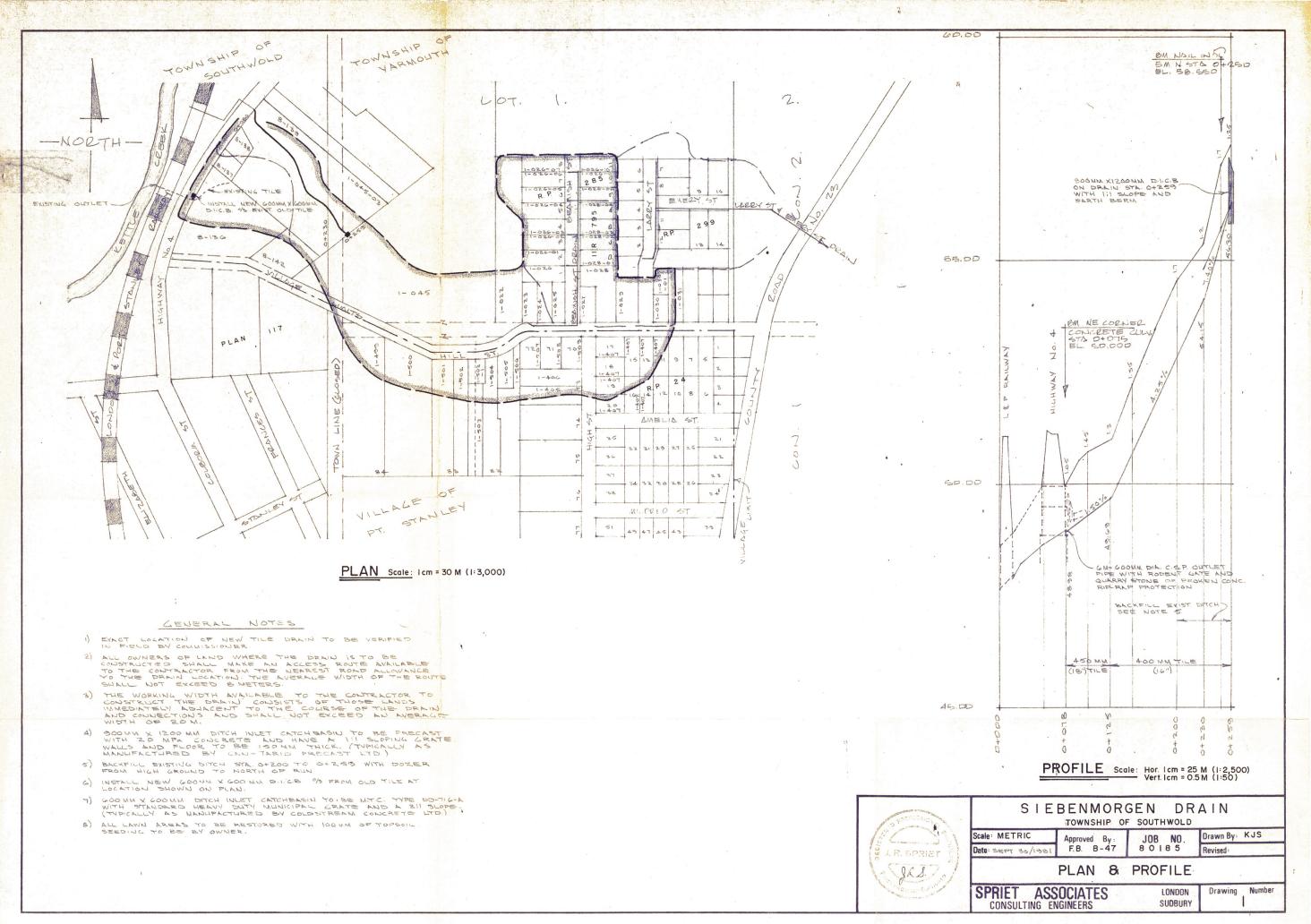
LIMIT OF WATERSHED AREA PROPOSED DRAINAGE WORKS EXTERIOR OR INTERIOR WATERSHED DRAIN BY TOUNSHIP EXIST. MUNICIPAL DRAIN

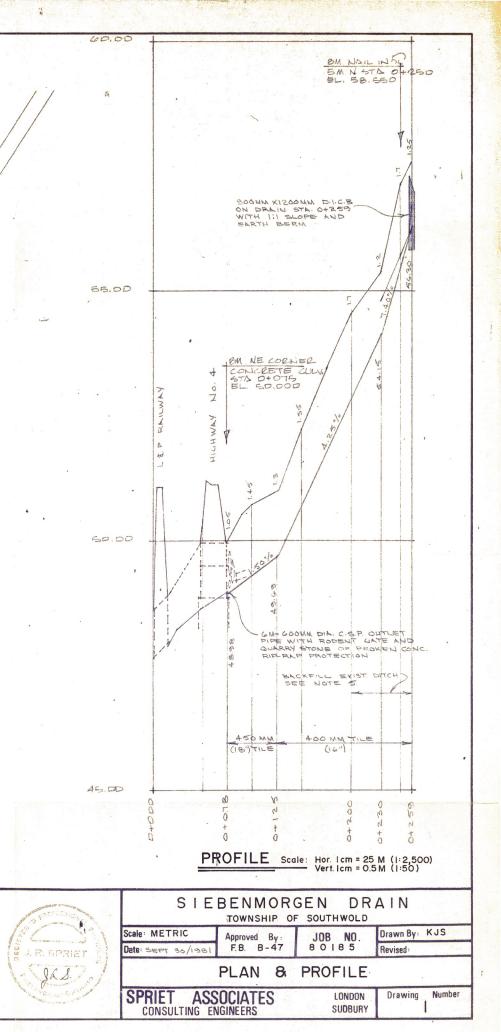




LIMIT OF WATERSHED AREA	
PROPOSED DRAINAGE WORKS	
EXTERIOR OR INTERIOR WATERSHED	
DRAIN BY TOUNSHIP	
EXIST. MUNICIPAL DRAIN	







<u>APPENDIX 'B' – STORMWATER MANAGEMENT CALCULATIONS</u>

279 HILL STREET PORT STANLEY, ON



Cyril J. Demeyere Limited P.O. Box 606, 261 Broadway Tillsonburg, Ontario. N4G 4J1 Tel: 519-688-1000 866-302-9886 Fax: 519-6842-3235 cjdleng@oxford.net

19084 29-Mar-22

PRE-DEVELOPMENT FLOW CALCULATIONS

				Item	Area (Ha)	C Value
TRIBUTARY AREA =	0.81 Ha			Gravel	0.03	0.70
RUNOFF COEF. =	0.3900			Building	0.04	0.95
				Sod	0.74	0.35
				Asph/Conc	0.00	0.85
				Agricultrual - Row Crop	0.00	0.25
PREDEVELOPMENT RUNOFF COEF.	=	0.3900		Total	0.81	0.39
Q = 0.0028*C*I*A			-			
$TC = (3.26 * (1.1-f*C)*(L)^{1/2})/Sw^{1/3}$			Intensity Factors	2 year	5 year	100 year
			a:	23.6	31.1	51.1
WATERSHED LENGTH (m)	150		b:	-0.699	-0.699	-0.699
WATERSHED SLOPE (%)	1					

Predevelopment Flows - 1 in 5 Year Storm Event

Rainfall Inter	sity MTO - IDF	Curve Lookup	
Intensity=a(t+b) ^{-c}	mm/hr		
a=	31.1		
b=	-0.699		
Intensity =	52.5 mm/hr		
Time of Concentration	C = (3.26 * (1.1-1.0*C)*(105	5)^1/2)/1.6^1/3 = 28.3	-
Predevelopment Flow (Qpre = 0.0028 * C * I * A =	46.5	l/s

Predevelopment Flows - 1 in 100 Year Storm Event

Rainfall Intens	sity MTO - IDF Curve Lookup	<u>)</u>
Intensity=a(t+b) ^{-c}	mm/hr	
a= 51	.1	
b= -0.	699	
Intensity =	95.7 mm/hr	
Time of Concentration TC	C = (3.26 * (1.1-1.25*C)*(126.31)^1/2)/1.25^1/3	3: 24.5
Predevelopment Flow Q	ore = 0.0028 * C * I * A =	105.8 l/s

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POST-DEVELOPMENT FLOW CALCULATIONS

RAINFALL STORAGE CALCULATIONS - 5 YEAR QUANTITY CONTROL

TRIBUTARY AREA =0.81 HaRUNOFF COEF. =0.70PRE-DEVELOP. MAX. OUTFLOW =46.5 l/sPOST-DEVELOP. MAX. OUTFLOW =41.6 l/s

Item	Area (Ha)	C Value
Gravel	0.00	0.70
Building	0.25	0.95
Sod	0.29	0.35
Asph/Conc	0.27	0.85
Agricultrual - Row	0.00	0.25
Total	0.81	0.70

Rainfall Intensity Intensity=a(t+b)^{-c} mm/hr

MTO - IDF Curve Lookup

	a=	31.1	Intensity Factors	2 year	5 year	100 year	
	b=	-0.699	a:	23.6	31.1	51.1	l
Total			b:	-0.699	-0.699	-0.699	l

	RAINFALL	TOTAL		MAX. RATE OF	VOLUME	VOLUME	I
TIME	INTENSITY	VOLUME	INFLOW	RELEASE	RELEASED	STORED	
[hrs]	[mm/hr]	[m^3]	[m^3/s]	[m^3/s]	[m^3]	[m^3]	
0.083	177.1	84	0.280	0.0416	12	71	
0.167	108.7	103	0.172	0.0416	25	78	←Max Storage required
0.333	67.1	127	0.106	0.0416	50	77	
0.50	50.5	144	0.080	0.0416	75	69	
0.667	41.3	157	0.065	0.0416	100	57	
0.833	35.3	167	0.056	0.0416	125	43	
1	31.1	177	0.049	0.0416	150	27	
1.5	23.4	200	0.037	0.0416	224	-25	
2	19.2	218	0.030	0.0416	299	-81	
3	14.4	246	0.023	0.0416	449	-203	
4	11.8	268	0.019	0.0416	598	-330	
8	7.3	331	0.011	0.0416	1197	-866	
12	5.5	374	0.009	0.0416	1795	-1421	
18	4.1	422	0.007	0.0416	2692	-2270	
24	3.4	460	0.005	0.0416	3590	-3130	

19084 29-Mar-22 Consulting Engineers

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19084 29-Mar-22

POST-DEVELOPMENT FLOW CALCULATIONS

RAINFALL STORAGE CALCULATIONS - 100 YEAR QUANTITY CONTROL

TRIBUTARY AREA =	0.81 Ha
RUNOFF COEF. =	0.88 (C Value x 125%)
PRE-DEVELOP. MAX. OUTFLOW =	105.8 l/s
POST-DEVELOP. MAX. OUTFLOW	65.9 l/s

Item	Area (Ha)	C Value
Gravel	0.00	0.70
Building	0.25	0.95
Sod	0.29	0.35
Asph/Conc	0.27	0.85
Agricultrual - Row	0.00	0.25
Total	0.81	0.70

Rainfall Intensity Intensity=a(t+b)^{-c} mm/hr

279 HILL STREET

PORT STANLEY, ON

MTO - IDF Curve Lookup

	a=	51.1	Intensity Factors	2 year	5 year	100 year
	b=	-0.699	a:	23.6	31.1	51.1
Total			b:	-0.699	-0.699	-0.699

	RAINFALL	TOTAL		MAX. RATE OF	VOLUME	VOLUME	
TIME	INTENSITY	VOLUME	INFLOW	RELEASE	RELEASED	STORED	1
[hrs]	[mm/hr]	[m^3]	[m^3/s]	[m^3/s]	[m^3]	[m^3]	1
0.083	291.1	172	0.575	0.0659	20	152	
0.167	178.5	212	0.352	0.0659	40	172	
0.333	110.2	261	0.218	0.0659	79	182	←Max Storage required
0.50	83.0	295	0.164	0.0659	119	176	
0.667	67.8	321	0.134	0.0659	158	163	
0.833	58.1	344	0.115	0.0659	198	146	
1	51.1	363	0.101	0.0659	237	126	
1.5	38.5	410	0.076	0.0659	356	55	
2	31.5	447	0.062	0.0659	474	-27	
3	23.7	505	0.047	0.0659	711	-206	
4	19.4	551	0.038	0.0659	948	-397	
8	11.9	679	0.024	0.0659	1897	-1218	
12	9.0	767	0.018	0.0659	2845	-2078	
18	6.8	867	0.013	0.0659	4268	-3401	
24	5.5	945	0.011	0.0659	5691	-4746	



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QUANTITY CONTROL REQUIREMENTS: 5YR STORM

ORIFICE PLATE 1

Q=CA $\sqrt{(2gH1)}$ d = $\sqrt{(4Q/(3.14C(v(2gH1))))}$

H1 = E1-E2

E1= 210.26	MAXIMUM PONDING ELEVATION
E2 = 209.87	CENTERLINE OF ORFICE OUTLET
H1 = 0.39	m
C = 0.85	CONSTANT
g = 9.81	GRAVITATIONAL CONSTANT

USE DIAMETER OF ORFICE (m)

Q= 0.0416 m³/s (Total)

QUANTITY CONTROL REQUIREMENTS: 100-YR STORM

ORIFICE PLATE 1

d= 0.150

Q=CA $\sqrt{(2gH1)}$ d = $\sqrt{(4Q/(3.14C(\sqrt{2gH1})))}$

H1 = E1-E2

E1= 210.85	MAXIMUM PONDING ELEVATION
E2 = 209.87	CENTERLINE OF ORFICE OUTLET
H1 = 0.98	m

- C = 0.85 CONSTANT
- g = 9.81 GRAVITATIONAL CONSTANT
- d= 0.150 USE DIAMETER OF ORFICE (m)

Q= 0.0659 m³/s (Total)

APPENDIX 'C' – STORMTECH SC-740 SWM CHAMBER DRAWINGS

PROJECT INFORMATION

ENGINEERED	CODY NEATH
PRODUCT	519-465-9958
MANAGER:	CODY.NEATH@ADS-PIPE.COM
ADS SALES REP:	ANDREW OKOLISAN 519-670-0564 ANDREW.OKOLISAN@ADS-PIPE.COM
PROJECT NO:	S224081



ADVANCED DRAINAGE SYSTEMS, INC.

279 HILL STREET PORT STANLEY, ON

SC-740 STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH SC-740. 1.
- 2. CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS
- CHAMBERS SHALL BE CERTIFIED TO CSA B184, "POLYMERIC SUB-SURFACE STORMWATER MANAGEMENT STRUCTURES", AND MEET 3. THE REQUIREMENTS OF ASTM F2418-16a, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD 4 IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- CHAMBERS SHALL BE DESIGNED, TESTED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2787, 6 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE: 1) INSTANTANEOUS (<1 MIN) AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2) MAXIMUM PERMANENT (75-YR) COVER LOAD AND 3) ALLOWABLE COVER WITH PARKED (1-WEEK) AASHTO DESIGN TRUCK.
- REQUIREMENTS FOR HANDLING AND INSTALLATION: 7
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 50 mm (2").
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 550 LBS/IN/IN. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 23° C / 73° F), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN ENGINEER OR OWNER. THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS:
 - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
 - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
 - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2418 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN EXCEPT THAT IT SHALL BE THE 75-YEAR MODULUS USED FOR DESIGN.
- CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY. 9

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-740 SYSTEM

- STORMTECH SC-740 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A 1 PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2.
- 3 CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 - STONESHOOTER LOCATED OFF THE CHAMBER BED.
 - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
 - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS. 4
- JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE. 5.
- MAINTAIN MINIMUM 150 mm (6") SPACING BETWEEN THE CHAMBER ROWS. 6.
- EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 20-50 mm (3/4-2"). 7.
- 8 THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE 9. STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- 1
- 2 THE USE OF CONSTRUCTION EQUIPMENT OVER SC-740 CHAMBERS IS LIMITED:
 - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".
- FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING. 3.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.



STORMTECH SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".

STORMTECH SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".

NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE

WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE"

CONCEPTUAL LAYOUT

78	STORMTECH SC-740 CHAMBERS
8	STORMTECH SC-740 END CAPS
152	STONE ABOVE (mm)
152	STONE BELOW (mm)
40	% STONE VOID
190.0	INSTALLED SYSTEM VOLUME (m ³) (PERIMETER STONE INCLUDED)
302.6	SYSTEM AREA (m ²)
185.7	SYSTEM PERIMETER (m)

CONCEPTUAL ELEVATIONS

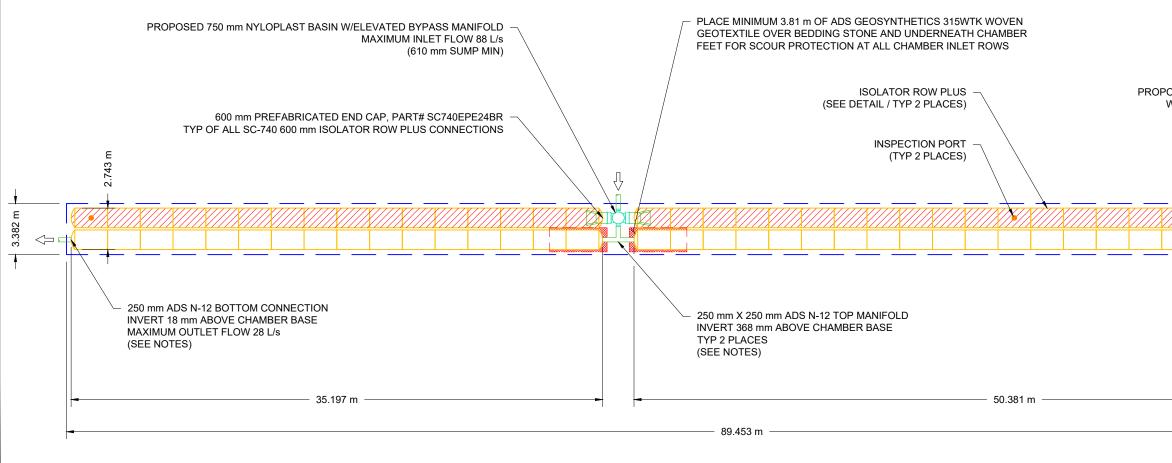
213.197	MAXIMUM ALLOWABLE GRADE (TOP OF PAVEMENT/UNPAVED):
211.369	MINIMUM ALLOWABLE GRADE (UNPAVED WITH TRAFFIC):
211.216	MINIMUM ALLOWABLE GRADE (UNPAVED NO TRAFFIC):
211.216	MINIMUM ALLOWABLE GRADE (BASE OF FLEXIBLE PAVEMENT):
211.216	MINIMUM ALLOWABLE GRADE (TOP OF RIGID PAVEMENT):
210.911	TOP OF STONE:
210.759	TOP OF SC-740 CHAMBER:
210.365	250 mm TOP MANIFOLD INVERT:
210.015	250 mm BOTTOM CONNECTION INVERT:
210.000	600 mm ISOLATOR ROW PLUS INVERT:
209.997	BOTTOM OF SC-740 CHAMBER:
209.845	BOTTOM OF STONE:

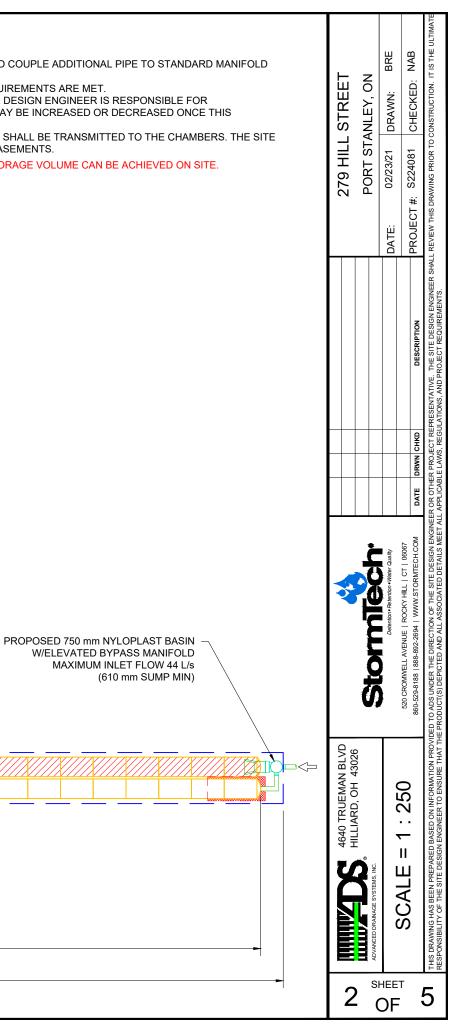
NOTES

MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECHNICAL NOTE 6.32 FOR MANIFOLD SIZING GUIDANCE.

DUE TO THE ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANIFOLD COMPONENTS IN THE FIELD.

- THE SITE DESIGN ENGINEER MUST REVIEW ELEVATIONS AND IF NECESSARY ADJUST GRADING TO ENSURE THE CHAMBER COVER REQUIREMENTS ARE MET.
- THIS CHAMBER SYSTEM WAS DESIGNED WITHOUT SITE-SPECIFIC INFORMATION ON SOIL CONDITIONS OR BEARING CAPACITY. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR DETERMINING THE SUITABILITY OF THE SOIL AND PROVIDING THE BEARING CAPACITY OF THE INSITU SOILS. THE BASE STONE DEPTH MAY BE INCREASED OR DECREASED ONCE THIS INFORMATION IS PROVIDED.
- THE SITE DESIGN ENGINEER MUST REVIEW THE PROXIMITY OF THE CHAMBERS TO THE BUILDING/STRUCTURE. NO FOUNDATION LOADS SHALL BE TRANSMITTED TO THE CHAMBERS. THE SITE DESIGN ENGINEER MUST CONSIDER EFFECTS OF POSSIBLE SATURATED SOILS ON BEARING CAPACITY OF SOILS AND SEEPAGE INTO BASEMENTS.
- NOT FOR CONSTRUCTION: THIS LAYOUT IS FOR DIMENSIONAL PURPOSES ONLY TO PROVE CONCEPT & THE REQUIRED STORAGE VOLUME CAN BE ACHIEVED ON SITE.





ACCEPTABLE FILL MATERIALS: STORMTECH SC-740 CHAMBER SYSTEMS

		MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPA	
	D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER.	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE INSTALL/	
	С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 18" (450 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMP THE CHAMBE 6" (150 mm) I WELL GRAI PROCESS VEHICLE WE	
	В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57		
	А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	PLATE CON	

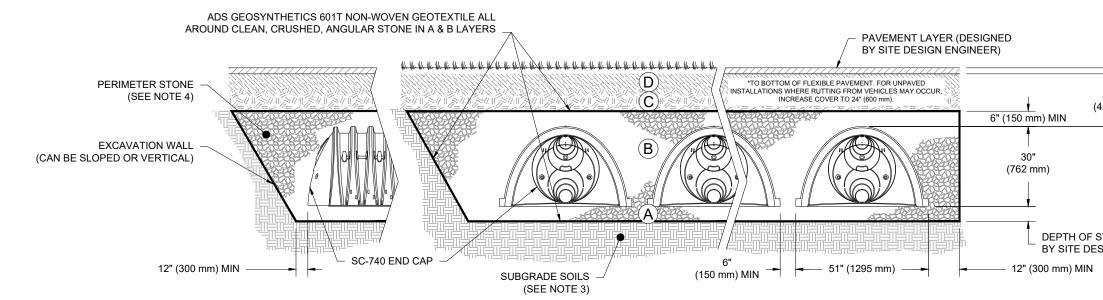
PLEASE NOTE:

1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".

2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 6" (150 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.

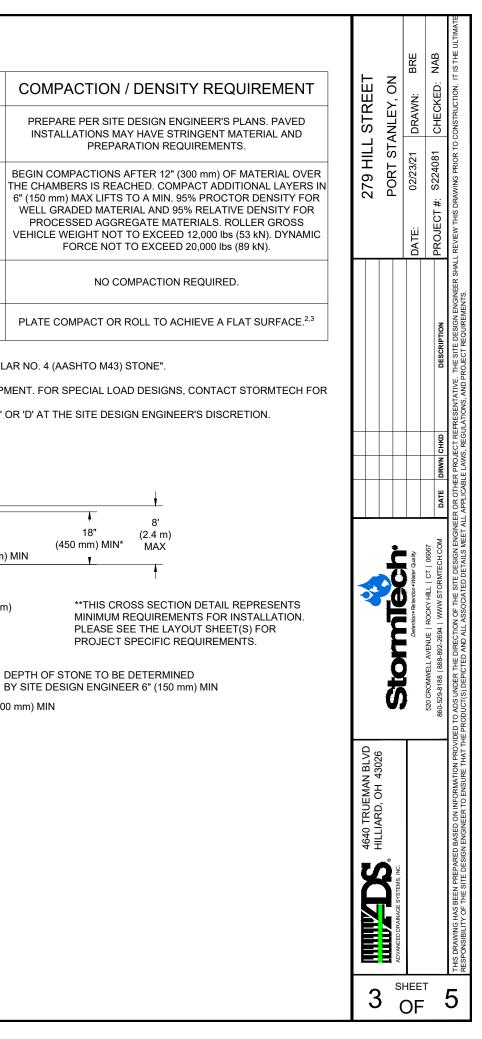
3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS.

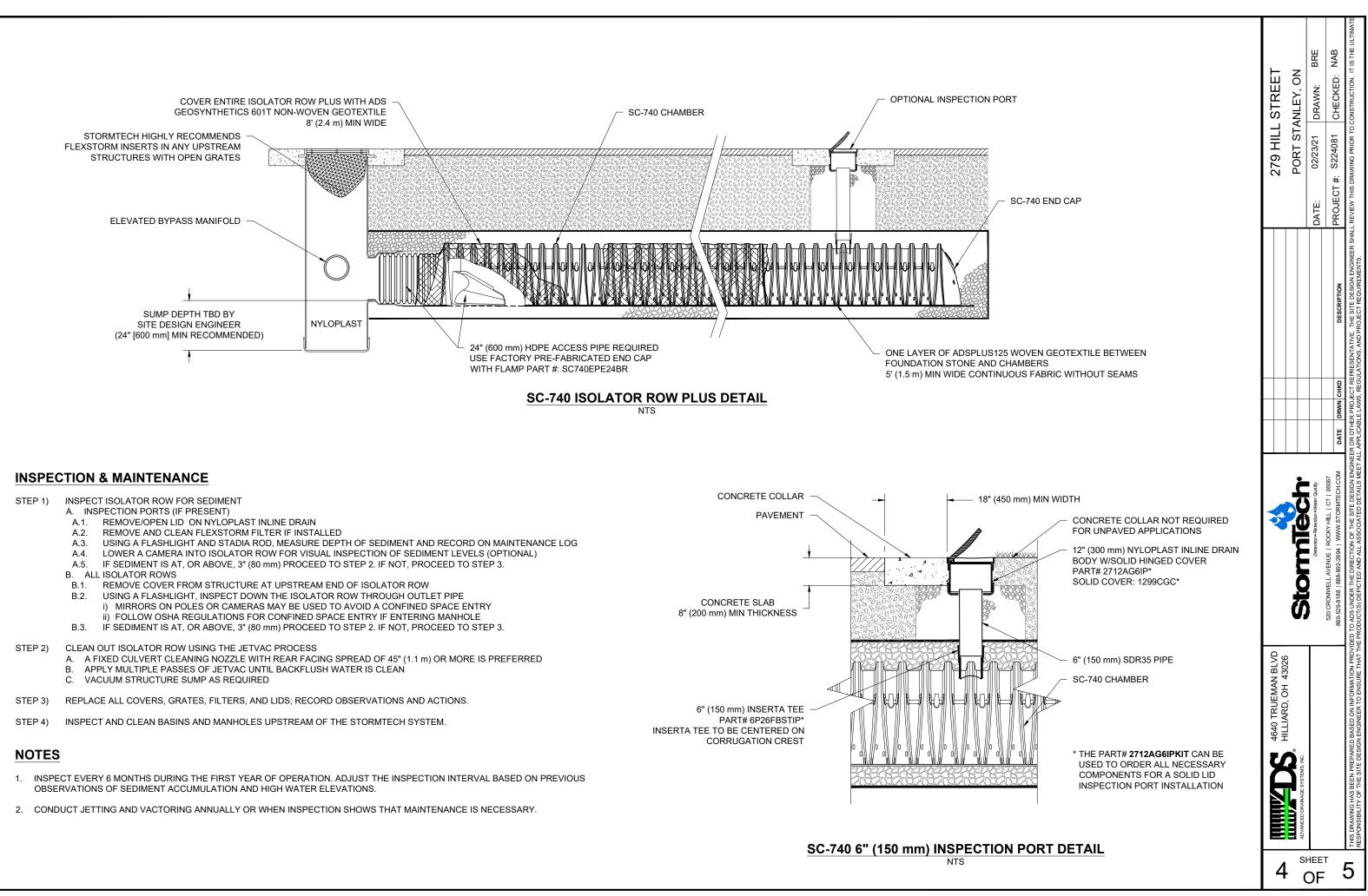
4. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.

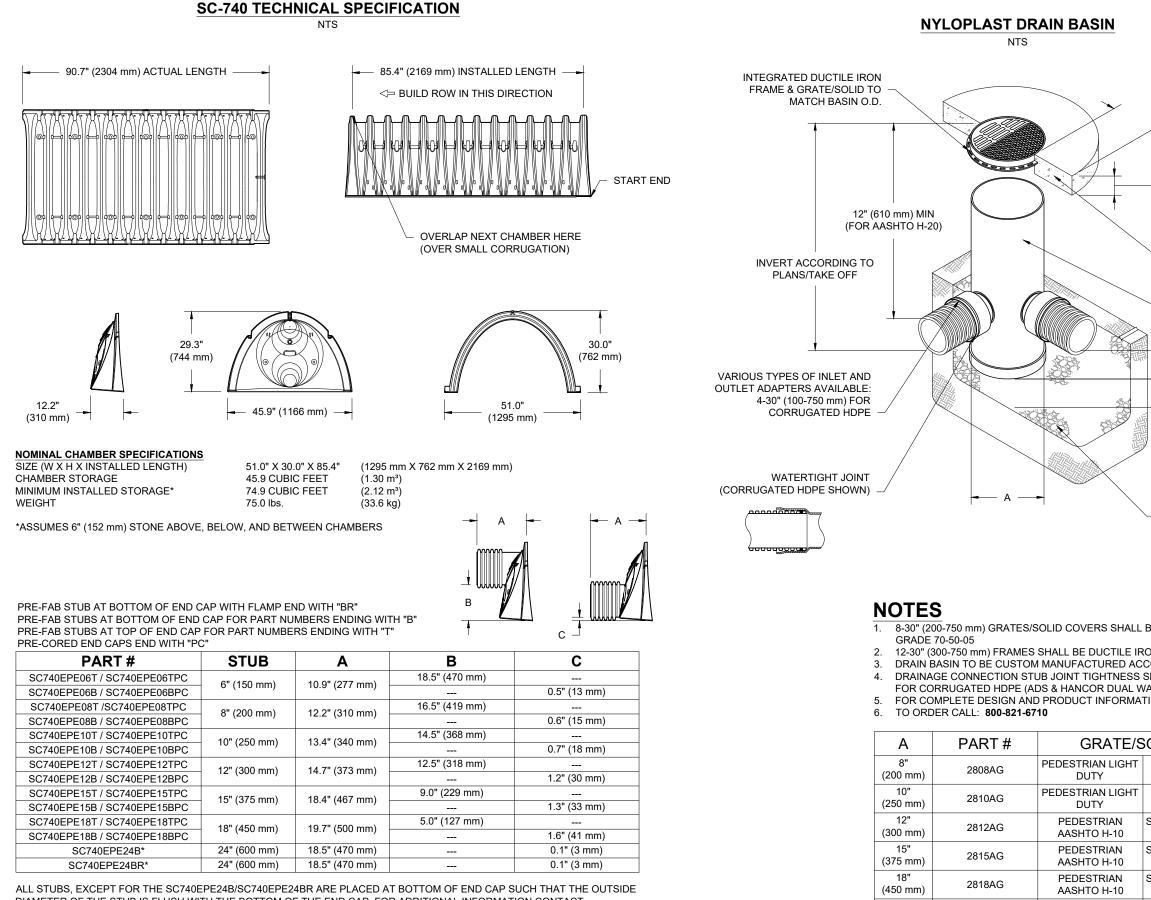


NOTES:

- 1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418-16a, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 2. SC-740 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 2".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 550 LBS/IN/IN. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.







24"

(600 mm)

30"

(750 mm)

2824AG

2830AG

PEDESTRIAN

AASHTO H-10

PEDESTRIAN

AASHTO H-20

DIAMETER OF THE STUB IS FLUSH WITH THE BOTTOM OF THE END CAP. FOR ADDITIONAL INFORMATION CONTACT STORMTECH AT 1-888-892-2694.

* FOR THE SC740EPE24B/SC740EPE24BR THE 24" (600 mm) STUB LIES BELOW THE BOTTOM OF THE END CAP APPROXIMATELY 1.75" (44 mm). BACKFILL MATERIAL SHOULD BE REMOVED FROM BELOW THE N-12 STUB SO THAT THE FITTING SITS LEVEL.

18" (457 mm) MIN WIDTH AASHTO H-20 CONCRETE SLAB 8" (203 mm) MIN THICKNESS TRAFFIC LOADS: CONCRETE DIMENSIONS ARE FOR GUIDELINE PUPOESS ONLY. ACTUAL CONCRETE SLAB MUST BE DESIGNED GIVING CONSIDERATION FOR LOCAL SOLIC CONTINUES (SAMUEL 9'- 360' ACCORDING & OTHER APPLICABLE DESIGN FACTORS AASHTO H-20 CONCRETE SUMP DEPTH ACCORDING & STHER APPLICABLE DESIGN FACTORS AACHACL CONCRETE SUMP DEPTH ACCORDING & OTHER APPLICABLE DESIGN FACTORS ACCORDING TO PLANS VARIABLE SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS Colors of the Concent of SUMP DEPTH ACCORDING TO PLANS TIT TANDARD LIGHT SOLID LIGHT DUTY IT STANDARD AASHTO ASSHTO ASSHTO ASSHTO H-20 STANDARD AASHTO ASSHTO ASSHTO H-20 STANDARD AASHTO ASSHTO SOLID H-20 AASHTO H-20 STANDARD AASHTO ASSHTO SOLID H-20 AASHTO H-20 STANDARD AASHTO ASSHTO ASSHTO ASOLID ACCORDING TO ASSHTO ASSHTO ASSHTO ASSHTO ASSHTO ASOLID ACCOR	VARIABLE SUMP DEPTH ACCORDING TO PLANS [6" (152 mm) MIN ON 8-24" (200-600 mm), 10" (254 mm) MIN ON 30" (750 mm)] 4" (102 mm) MIN ON 8-24" (200-600 mm) 6" (152 mm) MIN ON 30" (750 mm) 6" (152 mm) MIN ON 30" (750 mm) BACKFILL MATERIAL BELOW AND TO SIDES OF STRUCTURE SHALL BE ASTM D2321 CLASS I OR II CRUSHED STONE OR GRAVEL AND BE PLACED UNIFORMLY IN 12" (305 mm) LIFTS AND COMPACTED TO MIN OF 90%								ш
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